

In the Claims

Please cancel claims 1-19 and replace with new claims 20-44 as shown in Attachment 4, which new claims are formatted to conform to U.S. practice.

REMARKS

Reconsideration of this application as amended is requested. By this amendment Applicants have amended the drawing Figs. 1-3 and 6-8 as requested by the Examiner, have amended the specification as requested by the Examiner, and have replaced claims 1-19 with new claims 20-44. Claims 20-44 are in the case.

The Examiner objected to the drawing figures and the specification due to informalities, which have been corrected as indicated above and in Attachments 1-3. The Examiner also objected to claims 4-9 and 12-19 under 37 CFR 1.75(c) as being in improper form, which claims have been canceled and replaced by claims 20-44 in Attachment 4, rendering this objection moot.

The Examiner rejected claim 2 under 35 U.S.C. 112, first paragraph, as containing subject matter not described in the specification; rejected claims 1-3, 10 and 11 under 35 U.S.C. 112, second paragraph, as being indefinite; and rejected claims 1, 3, 10 and 11 under 35 U.S.C. 102(e) as being unpatentable over Phillips et al.

With the replacement of claims 1-19 with new claims 20-44 the Examiner's rejection under 35 U.S.C. 112, second paragraph, is deemed to be moot, and the new claims 20-44 are deemed to be allowable as being definite.

With respect to the rejection based on 35 U.S.C. 112, first paragraph, Applicants submit that the terms "Littrow system", "Ebert's array" and "array according to Faustie" are terms well-known to those of ordinary skill in the art. It is the purpose of the specification to teach one of ordinary skill in the art what is new, not what is already known. The Examiner is referred to <http://www.isainc.com/OSD/OOS/Theory%20of%20Optics%20and%20Spectroscopy.pdf>

"The Optics of Spectroscopy" by Lerner and Levinson, specifically sections 1.6.1 and 2.2 which deal with the Littrow condition and the Fastie-Ebert configuration, respectively. The Examiner also is referred to the "Diffraction Grating Handbook", 5th Ed. by Palmer in the library at <http://www.gratinglab.com/>. Therefore what constitutes a "Littrow system", and "Ebert's array" or a "Fastie" array is well known to those of ordinary skill in the optical arts, and the specification provides adequate support for the corresponding language in the new claims. Therefore claims 20-44 are deemed to be allowable as being supported by an enabling disclosure.

Reconsideration and allowance of claims 20-44 is requested over Phillips et al. The Examiner stated that Phillips et al teach (Fig. 1) a multi-wavelength system (col. 24, lls. 49-50) having a filter (220) provided in the form of a cross correlator (Abstract and col. 36, lls. 18-22); that Phillips et al teach a grating (49) provided for avoiding polarization-dependent reflections (col. 27, lls. 39-46); and that Phillips et al teach (Fig. 1) a non-linear opto-electronic component (102) as a photodiode (col. 7, lls. 39-42) for generating a working signal. Applicants respectfully traverse this improper and nonobvious conclusion by the Examiner.

In contradistinction to Applicants' claimed invention Phillips et al disclose a fiber-based ladar transceiver for range/doppler imaging using a frequency comb generator which is based on matched-filter cross-correlation of light pulse waveforms that have multiple, simultaneous frequency components with phase variation and incommensurate spectral frequency spacing between frequency components. A beam with many discrete frequency components, i.e., a broadband frequency spectrum, in randomized phase relations among the frequency components is transmitted in a long duration pulse. The pulse waveform is monitored and stored for subsequent matching with a return signal to determine simultaneously range and velocity of a target providing the return signal. The pulse waveforms (transmitted and return) are converted to electronic form by a photodiode and the matching is done of the digitized waveforms by a processor. The matched filters used for the auto-correlation between the transmitted and return signals are derived from the transmitted signal, and the auto-correlation is based on an iterative sequence of calculations based on a series of trial mathematical adjustments to the frequencies and phases of the transmitted signal until a best match with the return

signal is found. Phillips et al is not a DWDM optical communication system, but a laser radar. The purpose of Phillips et al is to determine range to and velocity of a target, not to parameterize or monitor the performance of a DWDM optical communication system.

Applicants specifically recite in claim 20 that "an optical signal for a particular wavelength from the DWDM multi-wavelength system" is converted to an electrical signal, whereas Phillips et al process the entire wide-band return signal without separating it into particular wavelengths. Applicants further recite that the electrical signal for the particular wavelength is processed "to determine the performance of the DWDM multi-wavelength system", and that the converting means is controlled "so that each particular wavelength of the DWDM multi-wavelength system is processed." Phillips et al neither teach nor suggest the processing of each particular wavelength within a multi-wavelength system, and Phillips et al does not determine the performance of a telecommunications system (DWDM multi-wavelength system) where each particular wavelength is a separate communications channel. Thus claim 20 and claims 21-44 dependent therefrom are neither anticipated nor rendered obvious to one of ordinary skill in the art by Phillips et al.

In view of the foregoing amendment and remarks allowance of claims 20-44 is requested, and such action and the issuance of this case are requested.

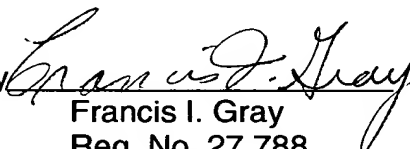
Respectfully submitted,

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TITLE OF THE INVENTION

System and Method for Monitoring the Performance of Dense Wavelength Division Multiplexing Optical Communication Services

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BACKGROUND OF THE INVENTION

The present invention relates to optical monitoring, and more particularly to a system and method of monitoring the performance of dense wavelength division multiplexing optical communication services.

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In densely packed WDM systems (dense WDM, DWDM) messages are communicated by light signals at different wave lengths via a single fiber only. Each wave length is the carrier of an information signal. All channels are within the wave length range from presently roughly 1,520 nm to 1,565 nm.

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The inter-channel separation amounts to a few nanometers or some hundreds of picometers, respectively. For standardization of these telecommunication systems, the international ITU- T Working Group has recommended the wave lengths (corresponding to the channels) to be used with an inter-channel separation of 100 GHz (≈ 0.8 nm) as standard. The ongoing development of these DWDM systems aims at the extension of the

20

utilizable wave length range up to 1,610 nm for example.

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Systems for the continuous monitoring of all characteristic parameters with the possibility of signal regeneration or improvement are required at many sites of this communication system. The most important parameters include the wave length and the capacity of all channels, the monitoring of the line width and the wave length drift of the lasers as well as the signal-to-noise ratio in each communication channel. Typical specification requirements for monitoring are:

- wave length measurement per channel with an absolute precision of 0.08 nm and a resolution of 0.01 nm,
- power metering per channel with an absolute precision of 0.4 dB and a resolution of 0.1 dB,
- 5 - S/N measurement between the channels with an absolute precision of 0.4 dB at 0.1 dB,
- reproducibility and a dynamic ratio of 33 dB at minimum,
- reliability over 10^{10} measuring cycles (20 years approximately),
- low PDL, (0.1 dB max.),
- 10 - small physical size.

Fundamentally different methods are suitable for monitoring purposes, which are employed in conventional optical spectrum analyzers.

Tunable narrow-band filters are used for wave length selection in the filtering technique. Acousto-optical filters (e.g. those produced by Wandel & Goltermann) or piezo-electrically controlled micro filters (e.g. those from the
15 Queensgate company) or tunable fiber Bragg gratings (e.g. those from ElectroPhotonics Corp.) are applied, which can be tuned directly via an electrical parameter.

The filtering technique is not only restricted to the optical filtering
20 operation but it may also be performed at the electrical signal level after a preceding conversion into electronic signals. With electronic filtering, the optical signal is mixed with an optical reference signal in a non-linear optical component while the differential frequencies are analyzed on an electronic spectral analyzer (Hewlett Packard Co.).

Another variant is the grating monochromator technique wherein either the grating is rotated or the spatially resolved signal spectrum is sensed by means of a single photodiode, or the grating is stationary and a scanning deflection mirror is provided in front of the exit slit of the monochromator, or a
5 mobile reflecting element varies the angle of incidence of the radiation on the grating (e.g. Photonetics company), or a stationary grating is used in combination with a line of photodiodes as detector unit (e.g. Yokogawa company).

10 In the interferometric technique, the spectrum is obtained from the detector signal of a Michelson interferometer with variable optical paths, with application of the Fourier transform (e.g. Hewlett Packard company).

None of the aforementioned conventional systems is suitable to satisfy the high demands made on a monitoring module for a DWDM system in terms of resolution, measuring accuracy, ASE measurement and dynamic
15 ratio, at the same time and in a suitable manner and to satisfy moreover the demands in terms of short measuring intervals, longevity and low space requirements as well as low-cost realization.

[The present invention is now based on the problem of implementing]
What is desired is a suitable measuring system that satisfies the demands on
20 a DWDM monitoring system in terms of resolution, measuring accuracy, ASE measurement and dynamic ratio, short measuring intervals, longevity and low space requirements as well as a low-cost production.

BRIEF SUMMARY OF THE INVENTION

In accordance with the present invention this object is achieved with a system permitting two variants. This aim is firstly reached in accordance with the invention with a narrow-band tunable band-pass filter in the form of a specific grating spectrometer permitting a high resolution and a high-speed sampling of the measured values according to Variant 1 [as illustrated in Fig. 1], and secondly the solution according to the present invention is presented in a Variant [according to Fig.] 2 as a purely electronic solution using an opto-electronic cross correlator.

The objects, advantages and other novel features of the present invention are apparent from the following detailed description when read in conjunction with the appended claims and attached drawing.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

Fig. 1 shows the fundamental structure of a narrow-band optical band-pass filter having a grating spectrometer and an analyzer unit.

Fig. 2 illustrates the principle of an opto-electronic cross-correlator.

Fig. 3 shows the principle of a grating spectrometer with multiple passages.

Fig. 4 illustrates an example of the structure and the optical path in the grating spectrometer with multiple passages.

Fig. 5 shows the structure of a position sensor.

Fig. 6 illustrates an example of an opto-electronic cross-correlator.

Fig. 7 illustrates a beam combination by means of fiber couplers.

Fig. 8 is a view of a dual-channel opto-electronic cross-correlator.

DETAILED DESCRIPTION OF THE INVENTION

Variant 1:

5 Fig. 1 illustrates the fundamental structure of the embodiment including a fiber input 5, a narrow-band tunable band-pass filter 1 and an analyzer 3. High-resolution spectrometers generally require several dispersive and imaging elements and are adjusted to the wave length to be detected in a complex manner.

10 An example of a system based on a multiple spectrograph is illustrated in Fig. 3. The measuring light arrives through a fiber optical waveguide 5 into the optical unit 13 including the spectrometer. The light selected by a particular wave length arrives from the optical unit 13 on the photo detector 11. The electrical signal obtained from the measuring light in the photo
15 detector is passed via a low-pass filter 6 to the signal processor 7. There the wave length is assigned which the reference unit 9 has determined from the position signal 8 of the position sensor 28 and which arrives at the signal processor 7, too. That processor generates also the necessary control signals for the driving unit 10 and the grating drive 12 that adjusts the wavelength-
20 determining element in the optical unit 13. The characteristic values of the instantaneously set wave length, which are calculated in the signal processor, are displayed to the user in the display unit 14 and made available for being passed on.

The problem to achieve a high resolution is solved, in accordance with Fig. 4, by the structure of a specific grating spectrometer 1 wherein an echelle or ruled grating or a blazed grating for the wave length range to be monitored is mounted in a combined array according to Ebert and Fastie and by
5 approximation in a Littrow array. The optical paths for the incident and exiting light are almost symmetrical there. Due to the multiple use of the grating and the single imaging element, that is equally provided for multiple use, in combination with several beam deflection systems composed of flat mirrors or prisms, a compact, stable, highly dispersive and low-cost structure is
10 achieved. A predominantly symmetrical optical path in the optical unit reduces imaging errors resulting in a dramatic impairment of the resolution. The movement of the grating for wave length selection can take place at a high speed because only a single element is moved. The application of a single detector element only prevents site-dependent or element-dependent
15 variations in the responsiveness. Moreover, a further-going independence from polarization effects such as PDL (polarization-dependent losses) is achieved because with the blazed grating or the ruled grating, respectively, the beams are incident on the diffracting grating surfaces almost orthogonally and cover a wide grating length at a high angle of incidence with a small
20 beam diameter.

The angular position of the dispersing grating, that is decisive for assigning the measuring wave length, is determined by means of an auxiliary means, the position sensor, according to Fig. 5.

For a general grating the fundamental equation

$$m\lambda = d(\sin \alpha + \sin \beta) \quad (I)$$

wherein m denotes the order, d represents the inter-line spacing and α , β indicate the angles of incidence or exit, respectively. As in a Littrow array
5 grating the angles of incidence and exit are almost identical, the definition according to Fastie furnishes the following simplified equation:

$$m\lambda = 2 d \sin \alpha \quad (II)$$

In the definition according to Ebert the basic equation (I) applies. The optical path of the beams is so designed that the most symmetrical optical
10 path possible will be available with respect to the concave mirror. As in this case, too, the angles of incidence or exit are almost equal, the angular dispersion comes also under a similar magnitude order as in the definition according to Fastie. Due to the multiple passages - here quadruplicate, for instance - of the radiation through the dispersive element the overall
15 dispersion and hence the resolution of the device is quadruplicated, too. On account of the utilization of mirror areas in symmetrical positions, the symmetrical optical path relative to the imaging concave mirror results in an extensive compensation of the imaging errors, particularly of astigmatism that leads to a substantial deterioration of resolution.

20 With a dielectric optical preliminary filter as band-pass element in the multiple optical paths any light of wavelengths beyond the DWDM range is suppressed. In such a case the filter is then passed only by the DWDM range, for instance, with a width of roughly 100 nm.

The detection of the entire spectrum is performed by a single radiation detector while the adjustment of the wave length to be detected is realized by rotating the grating about its vertical axis, which is performed both by motor drive means and by the configuration as spring-mass array with torsion bars, capable of oscillating.

Furthermore, the position of the grating is detected by a secondary laser with a very high precision. The focused beam of the secondary laser is directed onto a reflecting surface rigidly connected to the grating while the reflected beam is supplied to a position sensor including an incremental scale.

Fig, 4 illustrates an example of an appropriate embodiment. The light to be examined arrives through the entrance opening, that is configured as fiber input 25, into the optical system. The diverging optical path is shaped by the collimator and camera mirror 27 to achieve a parallel pencil that is passed on by approximation onto the grating 24 at the blaze angle. The diffracted pencil then arrives again at the collimator and camera mirror 27, is focused by the latter and arrives on the mirrors 21 and 22 where it is deflected in a way that now the pencil, which is divergent again, is passed, along an axis parallel with the axis of the collimator and the camera mirror 27. The parallel pencil then arrives at the grating 24 again, is diffracted there again and is incident on the collimator and camera mirror 27. From there, the beam is now directed to the mirror 15 and via the mirrors 16, 17 and 18. The beam has now reached a position above the optical axis and is incident again on the collimator and camera mirror 27, arrives from there again at the grating 24 and arrives via

the collimator and camera mirror 27 on the grating 24 a second time. From there, the beam, that is now dispersed even more strongly, arrives again at the collimator and camera mirror 27 and is passed from there to the mirrors 19 and 20, is incident on the collimator and camera mirror 27 again, then on the grating 24, and then on the collimator and camera mirror 27 for the last time. The focused and four times dispersed beam then arrives at the signal output 26. All beams arriving on the grating 24 several times and returned from there back to the collimator and camera mirror 27 again must pass through the dielectric band-pass filter 23 and are cut there to the useful frequency band.

Fig. 5 illustrates an example of a structure for detecting a position. The light of a secondary laser 41 is focused through the optical system 42 on the incremental scale 45. The rotation of the grating 43 and the involved rotation of the mirror 44 rigidly connected to the grating results in a deflection of the laser beam over the incremental scale 45.

The influence which the incremental scale takes on the laser intensity is detected by the joining detector 46 and made accessible for analysis.

Variant 2:

The Variant 2 according to Fig. 2 - an entirely electronic solution in the form of an opto-electronic cross correlator 2 - applies to methods known per se from high-frequency technology. In this case, however, two optical signals are mixed with each other without a previous conversion into electrical signals. These two signals are firstly the working light 5 to be examined and secondly the reference light originating from a tunable laser 4. When the

reference oscillator (laser) is tuned a beat frequency is created whose frequency decreases as it approaches the frequency of the working light; when the frequencies are equal it approaches zero. This permits the use of components envisaged for application in the low-frequency range and hence also for the mixer output of a high-impedance load resistor. This results in a substantial improvement of the responsiveness in detection. While the solutions known from the technique of optical superposition or interference operate usually on a load resistance of 50 Ohm, this array allows for the application of resistors of some kilo Ohm. The frequency range to be processed extends from a freely selectable lower frequency limit, that is expediently higher than interfering mains frequency and base band components caused by the modulation of intensity of the optical carriers, up to an upper frequency limit which determines the bandwidth of integration. This frequency is expediently not substantially lower than the spectral width of the tunable laser acting as local oscillator. The advantage of such a system resides in the compact design, in the omission of mobile parts, in a purely electronic solution using components appropriate for application in the low-frequency range, in the measuring rate restricted only by the tuning speed of the reference oscillator, and in a high responsiveness at an almost optionally small bandwidth of analysis.

The two light signals are defined by the following two relationships:

$$\begin{aligned} \mathbf{E}_M &= E_M [i \int_{0 \rightarrow t} \omega t dt] e_M \\ \mathbf{E}_R &= E_R [i \int_{0 \rightarrow t} \Omega t dt] e_R \end{aligned}$$

This results in the following photo-electric current:

$$\begin{aligned} I &= | \mathbf{E}_M + \mathbf{E}_R |^2 \\ &= \mathbf{E}_M \cdot \mathbf{E}_M + \mathbf{E}_R \cdot \mathbf{E}_R + 2 \operatorname{Re} \{ \mathbf{E}_M \cdot \mathbf{E}_R \} \\ &= E_M^2 + E_R^2 + 2 E_M E_R \cos \left[\int_{0 \rightarrow t} (\omega - \Omega) t dt \right] \end{aligned}$$

It is apparent that the last term defines a current variable in time, that
5 is dependent on the amplitudes of both radiations and on the difference of the
light frequencies. When both frequencies are approaching each other a low-
frequency signal is created with the maximum amplitude $I_{\max} = 2 E_M E_R$.
Moreover, the direction of polarization of both light sources is equally
considered. In order to eliminate this dependence, it is possible, on the one
10 hand, to render the reference light laser or the source of working light
statistically variable in terms of its direction of polarization, or, on the other
hand, to make two orthogonally polarized beams
available, for instance, as reference light sources while the optical mixture is
performed in two separate detectors with a subsequent logic operation in the
15 signal processor. For another solution, for example, it is possible to switch the
reference laser over in a time-sequential manner in the polarization plane
while the subsequent measurements in succession are subjected to a logic
operation in the signal processor.

Fig. 6 shows an example of Variant 2. The radiation to be measured
20 arrives as working beam via the fiber input 5 on a non-linear optical
component, the detector 32. At the same time, the reference beam 40 is
passed via the polarizer 47 to the detector 32. The electrical mixed products
generated from the optical signals arrive via the low-pass filter 33 to the
rectifier 34 and from there at the digital signal processor 35 which realizes the

evaluation of the signals, controls the display unit 36 and supplies the reference laser controller 37 by means of the tunable laser 38.

By employment of the wave length calibrator 29 for wave length assignment the provision of wave length references is made possible in both
5 variants. To this end known arrays such as absorption cells are suitable for this purpose, which contain gases displaying characteristic lines of absorption in the required wave length range. When such a cell is inserted into the optical path, for instance in the spectrometer, and when the system is exposed to wide-band illumination characteristic signal developments are
10 created which permit a precise assignment of the wave lengths. Another possibility is the measurement of the reference laser wave length by means of an additional interferometer array. In such a system, one part of the light from the tunable reference light laser is passed on to an interferometer that is provided with a supplementary highly precise light source and in which the
15 interference signals [variable] vary in time, which are generated when the reference light laser is tuned, serve to assign the wave length present in that moment.

The combination of the working light and the reference light can be realized in different manners. Fig. 6 illustrates the free irradiation with the
20 measuring light, the reference light and possibly the calibration light, which are incident on the non-linear detector component 32.

Fig. 7 shows that the various beams are combined by means of a fiber optical component that is implemented in the form of a bulk or Y-type fiber coupler 48. The working signal at the fiber input 31 arrives via the coupler 48

at the detector 32. The light of the reference laser 38 is combined with the light of the wave length calibrator 29 via the polarizer 47 in another coupler 48 and added to the working light in a first coupler 48.

Fig. 8 illustrates an example of a dual-channel design permitting the consideration of the aforementioned dependence on polarization. The working light is subdivided into two channels of orthogonal polarization by means of a polarizing beam splitter 49. The reference laser 38 is equally split into two beams of orthogonal polarization and passed, together with the associated working beams, to two separate detectors 46. The output signals of both detectors then arrive at the signal processor 35 where they are processed.

[PATENT] CLAIM OR CLAIMS

WHAT IS CLAIMED IS:

1. System for monitoring the performance of DWDM multi-wavelength
5 systems, characterized in that a narrow-band and tunable low-pass
filter (1) for the DWDM range is provided in a purely electronic form
based on the principle of opto-electronic mixing in the form of a cross
correlator (2).
2. System according to Claim 1, characterized in that the grating (24) in
10 the form of a Littrow system both in the form of Ebert's array and in the
form of an array according to Fastie is disposed for the multiple
passage.
3. System according to Claim 1 or 2, characterized in that a grating is
provided which is a ruled grating for avoiding polarization-dependent
15 reflections, and which ensures an almost orthogonal incidence on said
grating (24).
4. System according to the Claims 1 to 3, characterized in that a dielectric
preliminary filter (22) is provided for suppressing wave lengths beyond
the working range, which, due to the multiple passage, multiplies its
20 efficient quality.
5. System according to Claim 4, characterized in that said grating (24) is
provided for both a rotational movement and a periodically oscillating
movement for wave length adjustment.
6. System according to Claim 5, characterized in that the combination of

a moved grating (24) with an optical position sensor (28) is provided.

7. System according to the Claims 1 to 6, characterized by a secondary laser (41) for scanning the moving object in order to derive a synchronizing signal for wave length assignment of the output signal of the system.

8. System according to the Claims 1 to 8, characterized by a position sensor (28) for deriving a position signal (8) of the moving object.

9. System according to the Claims 1 to 8, characterized in that said position sensor (28) consists of a line-shaped photodiode (46) with an incremental scale (45) disposed in front of it.

10. System according to Claim 1, characterized in that for optically mixing two optical signals for the generation of a working signal, a non-linear opto-electronic component (30) is provided.

11. System according to Claim 1 or 10, characterized in that said non-linear opto-electronic component (30) is a photodiode (32).

12. System according to Claim 1, 10 or 11, characterized in that said photodiode (32) is provided for being directly irradiated from both light sources (39, 40) for combining the optical signals.

13. System according to Claim 1, 10 or 11, characterized by a bulk or fiber optical Y -type coupler (48) for combining the optical signals.

14. System according to Claim 1 or Claims 10 to 13, characterized in that said electronic mixed signal is within the range of the low-frequency band.

15. System according to Claim 10 or Claims 10 to 14, characterized by a signal processor (35) for processing, rectification and further analysis of the low-frequency useful signal.
16. System according to Claim 1 or Claims 10 to 15, characterized by a tunable laser (38) for generating the reference radiation.
17. System according to Claim 1 or Claims 10 to 16, characterized in that said tunable laser (38) is a diode laser or a fiber laser.
18. System according to Claim 1 or Claims 10 to 17, characterized by a laser (38) that is commutable in increments and finely tunable within each segmental range for generating said reference radiation.
19. Method of monitoring the performance of DWDM multi-wavelength systems, characterized in that a system according to Claims 1 to 18 is applied.

[List of the Figures

Fig. 1 shows the fundamental structure of a narrow-band optical band-pass filter

consisting of a grating spectrometer and an analyzer unit

5 Fig. 2 illustrates the principle of the opto-electronic cross correlator

Fig. 3 shows the principle of the grating spectrometer with multiple passages

Fig. 4 illustrates an example of the structure and the optical path in the grating spectrometer with multiple passages

Fig. 5 shows the structure of the position sensor

10 Fig. 6 illustrates an example of an opto-electronic cross correlator

Fig. 7 illustrates the beam combination by means of fiber couplers

Fig. 8 is a view of a dual-channel opto-electronic cross correlator.

Legend of the Figures

	1	grating spectrometer
	2	opto-electronic cross correlator
	3	analyzer
5	4	reference oscillator, laser, reference laser
	5	input signal, fiber optical waveguide, fiber input
	6	low-pass filter
	7	signal processor
	8	position signal
10	9	reference unit
	10	driving unit
	11	photo detector, photodiode
	12	grating drive
	13	optical unit
15	14	display unit
	15	mirror
	16	mirror
	17	mirror
	18	mirror
20	19	mirror
	20	mirror
	21	mirror
	22	mirror
	23	dielectric preliminary filter, dielectric band-pass filter

	24	grating
	25	input, fiber input.
	26	output
	27	collimator and camera mirror
5	28	position sensor
	29	wave length calibrator
	30	non-linear opto-electronic component
	31	fiber input
	32	detector, non-linear detector component, photo diode
10	33	low-pass filter
	34	rectifier
	35	signal processor
	36	display unit
	37	reference laser controller
15	38	tunable laser, reference laser
	39	working beam
	40	reference beam
	41	secondary laser
	42	optical system
20	43	grating
	44	mirror
	45	incremental scale
	46	detector, line-shaped photo diode
	47	polarizer

- 48 bulk or Y -type fiber coupler
- 49 polarizing beam splitter]

[Abstract of the Disclosure] ABSTRACT OF THE DISCLOSURE

[System and Method for Monitoring the Performance of Dense Wavelength

Division

Multiplexing Optical Communication Services]

5 [The invention relates to a] A system and [a] method for monitoring all
the characteristic parameters of a DWDM communication system[.
In accordance with the invention this] is implemented with two variants.
Firstly, this is achieved by means of a specific grating spectrometer [1]
displaying a high resolution and a high-speed sampling of the measured
10 values, and secondly by the application of an opto-electronic cross correlator
[2] as a purely electronic solution. The grating spectrometer [1] is expediently
a particular system in a mixed array according to Ebert and Fastie, wherein
the light to be measured passes four times through the grating in a specific
manner. The opto-electronic cross correlator [2] can mix the working light
15 with a reference light tunable in terms of its frequency to form an electrical
low-frequency signal that is analyzed in a high-impedance operation.